

Study of a Parabolic Trough Adequate for the CERER Site (Dakar-Senegal)

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Abstract: This study presents the modeling of a parabolic trough solar collector. The main objective is to show the influences of the parabolic trough sensor effective efficiency (concentrator optical efficiencies of transmission, reflection, geometrical and the receiver absorption coefficient), of its length, of the mass flow rate on temperatures distributions of the heat fluid and the receiver and on thermal global efficiency (solar conversion efficiency into energy usable). The atmospheric parameters are those of Senegal in April. A prototype existing in the CERER (Center of Studies and Research on Renewable Energies) (Dakar-Senegal) is given as example of application.

Key words: Parabolic trough solar collector, receptor, efficiency, temperature, fluid.

Nomenclature

Bi	Biot number
$c_{p, f}$	Specific mass heat capacity at constant pressure
D	Hydraulic diameter of the absorber tube
F	Shape factor
Gz	Graetz number
h_{conv}	Coefficient of forced convection of the heat fluid
h_v	Coefficient of external mixed convection
DNI	Direct normal insolation
l_{conc}	Width of the concentrator
l_r	Perimeter of receiver tube
L_{conc}	Length of the concentrator
\dot{m}	Mass flow rate of the fluid
P_m	Wetted perimeter of the absorber tube
Pr	Prandtl number
\dot{Q}_{conc}	Thermal power emitted by the concentrator and received by the receiver
\dot{Q}_{conv}	Thermal power lost by convection
\dot{Q}_f	Thermal power received by the heat fluid

\dot{Q}_r	Thermal power transmitted from the receiver to the engine heat exchanger
\dot{Q}_{ray}	Thermal power lost by radiation
\dot{Q}_s	Thermal power emitted by the sun and received by the concentrator
Re	Reynolds number
S	Fluid passage section
S_{conc}	Opening surface of the concentrator
S_m	Wetted surface of the receiver tube
S_r	Surface of receiving envelope
t	Time
T_0	Ambient temperature
T_f	Average temperature of the heat fluid in the tube
$T_f(x)$	Local temperature of the heat fluid
T_{in}	Input temperature of the heat fluid in the tube
T_{out}	Output temperature of the heat fluid in the tube
T_p	Average temperature of the wall of the receiver tube
$T_p(x)$	Local temperature of the wall of the receiver tube
T_r	Average temperature of the receiving envelope
$U(r)$	Component of the velocity of the heat fluid depending to x
$\langle U \rangle$	Average velocity of the heat fluid
v	Wind velocity

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α_{conc}	Geometric concentration ratio $\alpha_{conc} = \frac{S_{conc}}{S_r}$
α_r	Absorption coefficient of the receiver tube
ε	Emissivity coefficient of the receiver tube
ζ_{conc}	Geometrical efficiency of the concentrator
κ_{PT}	Effective efficiency of the PT (parabolic trough)
λ	Thermal conductivity of the fluid
μ	Dynamic viscosity of the fluid
η_{conc}	Optical efficiency of the concentrator
η_{th-PT}	Thermal global efficiency of the PT
ρ_{conc}	Optical efficiency of reflection
σ_{SB}	Stefan Boltzmann constant
τ_{conc}	Optical efficiency of transmission

1. Introduction

In developing countries like Senegal, the production of clean energy that promotes sustainable development alternative to depletable energy sources such as gas or oil is a major issue. Currently the only technological responses to this requirement are the use of generators consuming fossil fuels or photovoltaic cells associated with batteries [1]. Solar thermal energy consists in using the heat from the solar radiation to heat a fluid at high temperature rather than the radiation itself. If the fluid temperature is so high, it can then activate a thermodynamic cycle to generate electricity. This sector is that of the concentrated solar power. The Sahelian-sub-Saharan countries with a favorable geographical location have a real solar potential with nearly 3,000 hours/year of radiation to reach high temperatures that remain unavoidable for solar energy production by thermodynamic way. One of the selective criteria is a simple technology to realize and its performances and costs able to be competitive with photovoltaic systems [2].

Specific components of concentrated solar power system are generally: the concentrator or collector, the receiver, the thermodynamic cycle and possibly a thermal storage or hybridization. The insulations are concentrated on a horizontal receiving tube in which circulates a heat transfer fluid whose temperature usually reaches 673 K. This fluid is then

pumped through heat exchangers to produce superheated steam which activates a turbine or an electric generator [3].

This study is about the sensor relative to the concentration of solar radiation. It is where is done the thermal conversion of solar radiation into usable heat. Its performances determine the overall efficiency of the solar power plant [4]. In order to proceed to an energy analysis of the PT (parabolic trough), a realistic model allowed to focus on temperatures distributions of the heat fluid and the receiver and on thermal global efficiency (solar conversion efficiency into energy usable) according on the parabolic trough effective efficiency, its length and the mass flow rate. Solar tangor sensor is designed by way of application.

2. Analytical Modelling

The parabolic trough is constituted by an absorbent cavity with superficial treatment with very high absorption and heat-thin allowing to neglect the thermal conduction [5]. The absorber is protected by a coaxial borosilicate envelope tube with stagnant air and very low iron content which prevents the dispersion of heat into the atmosphere, suggesting that the temperature of the receiving envelope is equal to the temperature of the wall of the receiver tube, $T_r = T_p$. The whole, called receiver is placed on the optical focal axis of a specular parabolic curved solar reflector at very high degree of reflection. The concentrator focuses the DNI (direct normal insolation) towards the receiver to allow it reaching high temperatures [6]. The collector is oriented north-south and tracks the sun continuously. To find temperatures fields of the heat fluid and the receiver wall, we start from the energy balance equation on a volume element at the receiver tube.

We recognize that:

- The inertia effects of the absorber and the fluid (considered as an ideal gas with constant physical properties) are negligible;

- The absorber is heat-thin ($Bi < 0.1$);
- The optical efficiency of the concentrator η_{conc} considered is independent of the concentration geometrical ratio α_{conc} .

$$\eta_{conc} = \tau_{conc} \rho_{conc} \zeta_{conc} \quad (1)$$

where, τ_{conc} is optical efficiency of transmission, ρ_{conc} is optical efficiency of reflection, ζ_{conc} is geometrical efficiency of the concentrator.

To find the equation that governs the operation of the heat absorber, we assume energy balance on the elementary surface $dS = 2\pi R dx$ of the tube. It comes then:

$$\dot{Q}_{conc} = \dot{Q}_{conv} + \dot{Q}_{ray} + \dot{Q}_f \quad (2)$$

With:

$$\dot{Q}_{conc} = \alpha_r \eta_{conc} DNI \cdot S_{conc} \quad (3)$$

$$\dot{Q}_{ray} = \sigma F \varepsilon S_r (T_r^4 - T_0^4) \quad (4)$$

$$\dot{Q}_f = h_{conv} S_m (T_p(x) - T_f(x)) \quad (5)$$

$$\dot{Q}_{conv} = h_v S_r (T_r(x) - T_0) \quad (6)$$

Supposing that $T_r(x) = T_p(x)$, we obtain:

$$\begin{aligned} \kappa_{PT} DNI \cdot l_{conc} &= h_{conv} P_m (T_p(x) - T_f(x)) \\ &+ h_v l_r (T_p(x) - T_0) \\ &+ \varepsilon \sigma F l_r (T_p(x)^4 - T_0^4) \end{aligned} \quad (7)$$

where, T_0 is the ambient air temperature, $\kappa_{PT} = \alpha_r \eta_{conc}$ is the PT effective efficiency, depend only on the PT intrinsic characteristics.

$T_f(x)$ is the average temperature of the fluid in the abscissa x defined by:

$$\langle U \rangle T_f(x) =$$

$$\frac{1}{\pi R^2} \iint_{r=0, \theta=0}^{r=R, \theta=2\pi} U(r) \cdot T_f(r, \theta, x) r dr d\theta \quad (8)$$

Supposing that, the flow is hydro-dynamically established and unidirectional transfers. Under these conditions, the integration of the heat equation in the elementary volume $dV = \pi R^2 dx$ leads to:

$$\dot{m} c_{p, f} \frac{dT_f}{dx} = h_{conv} P_m (T_p(x) - T_f(x)) \quad (9)$$

Thus the PT operating is governed by the following system of equation:

$$\begin{cases} \kappa_{PT} DNI \cdot l_{conc} = h_{conv} P_m (T_p(x) - T_f(x)) \\ \quad + h_v l_r (T_p(x) - T_0) \\ \quad + \varepsilon \sigma F l_r (T_p(x)^4 - T_0^4) \\ \dot{m} c_{p, f} \frac{dT_f}{dx} = h_{conv} P_m (T_p(x) - T_f(x)) \end{cases} \quad (10)$$

The exchange coefficient by forced convection h_{conv} for an internal flow is defined by:

$$h_{conv} = \frac{\lambda Nu}{D} \quad (11)$$

Several correlations are supposed depending on the cases of air flow in a circular tube of finite length with:

If $Re < Rec$, laminar flow;

If $Gz < 100$, we use Hausen relation [7]:

$$Nu = 3.66 + \frac{0.0668 Gz}{1 + 0.04 (Gz)^{2/3}} \quad (12)$$

If $Gz > 100$, we use Sieder and Tate relation [7]:

$$Nu = 1.6 (Gz)^{1/3} \quad (13)$$

If $Re > Rec$, turbulent flow we use Dittus-Boelter relation [7]:

$$Nu = 0.023 Re^{0.8} Pr^{0.4} \quad (14)$$

With:

$$Pr = \frac{c_p \mu}{\lambda} \quad (15)$$

$$Re = \frac{\dot{m} D}{\mu S} \quad (16)$$

$$Gz = Re \cdot Pr \cdot \frac{D}{L} \quad (17)$$

To solve the problems of atmospheric air in contact with horizontal walls, the McAdams and Woertz formulation is the most used [8]:

$$h_v = 3.86V + 5.67 \quad (18)$$

Supposing:

$$\dot{Q}_s = DNI \cdot S_{conc} \quad (19)$$

$$\dot{Q}_r = \dot{Q}_{conc} - h_v S_r (T_r - T_0) - \sigma_{SB} F \varepsilon S_r (T_r^4 - T_0^4) \quad (20)$$

$$\eta_{th-PT} = \frac{\dot{Q}_r}{\dot{Q}_s} \quad (21)$$

The differential Eq. (9) was integrated owing to a predictor-corrector scheme (Heun scheme) of second order [9]. The iterative Newton-Raphson method is

used to solve the non-linear Eq. (10) because of the term T^4 .

3. Results and Discussions

This study was realized on the site of the CERER (Center of Studies and Research on Renewable Energies) in Dakar Hann Equipe (Senegal) located by the following geographical coordinates: $14^{\circ}43'11''$ North, $17^{\circ}26'24''$ West and 35 m of elevation.

Contrary to the flat plate solar collectors that benefit from global solar radiation, the main input variable of any CSP (concentrated solar power) system is the DNI [10]. By satellite measurements, the atlas data PVGIS (photovoltaic geographical information system) allowed us to estimate the site's energy potential [11]. The ambient temperature T_0 and the wind velocity set respectively at 300 K and $5 \text{ m}\cdot\text{s}^{-1}$ are the usual climatic conditions in Dakar, the DNI is equal to $799 \text{ W}\cdot\text{m}^{-2}$.

3.1 Influences of the PT Intrinsic Characteristics

The variations of the output temperature T_{out} and the thermal global efficiency η_{th-PT} (solar conversion efficiency into energy usable) depending on the PT effective efficiency κ_{PT} are shown in Fig. 1.

The output temperature of the fluid T_{out} increases with the coefficient κ_{PT} . Just as the PT thermal global efficiency η_{th-PT} which follows a linear form:

$$\eta_{th-PT} = a \cdot \kappa_{PT} \quad (22)$$

$$a \approx 0.2$$

Indeed, losses caused by the geometrical defects must be as low as possible to maximize the performances of the PT. Similarly the optical efficiency of reflection ρ_{conc} , which determines the quantity of radiation received by the receiver, compared to the incident radiation on the concentrator must be optimized. The transmission factor τ_{conc} and absorption coefficient α_r should be improved.

For this, the blocks of reflective surfaces must be well assembled and set moving in order to track the sun. To reach high temperatures, it is necessary to

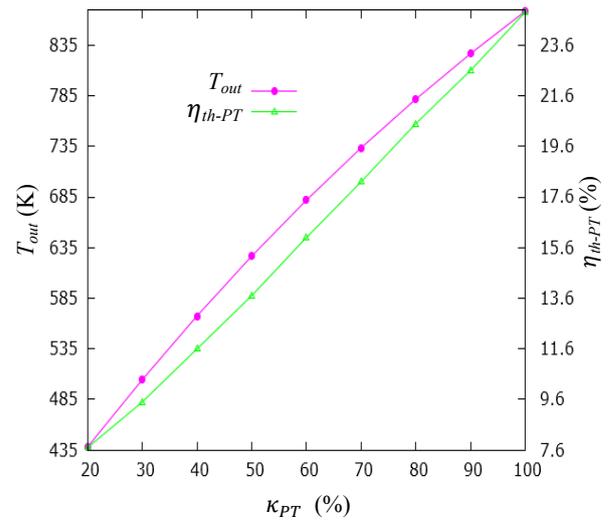


Fig. 1 Variations of T_{out} and η_{th-PT} according to κ_{PT} with $\dot{m} = 0.001 \text{ kg}\cdot\text{s}^{-1}$.

concentrate the radiation by a surface with extreme reflectivity with a best technico-economic compromise [12].

In order to increase the temperature of the heat fluid, it is necessary to isolate the absorber with a glass envelope while leaving the concentrated radiation to return. The glass prevents the diffused rays to leave by performing "the greenhouse effect". Fragile glass can be replaced by some polymer film [13]. But the major disadvantage of these materials is the deterioration of their properties under the effect of the ultraviolet rays. To improve the heat transfer, the absorber must have a high coefficient of absorption and be painted in perfect black. They are also investigations on potential of using two tubular receivers in one compound parabolic concentrator [14].

3.2 Influences of the PT Length

Fig. 2 represents temperatures progression of the wall receiver tube T_p and of the heat fluid T_f according to the concentrator length L_{conc} , its width l_{conc} being fixed.

We note that, the temperature profiles are on this form:

$$T_i(L_{conc}) \approx \frac{T_i(0)}{1-a_i} \cdot [1 - a_i \cdot e^{-b_i \cdot L_{conc}}] \quad (23)$$

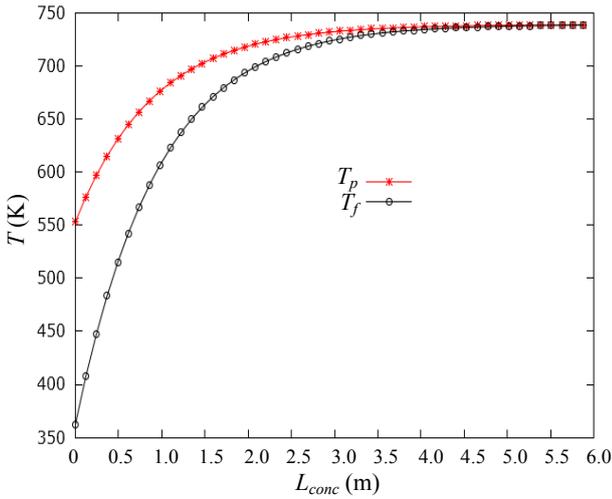


Fig. 2 Evolutions of temperatures T_p and T_f according to L_{conc} with $\dot{m} = 0.001 \text{ kg}\cdot\text{s}^{-1}$.

(i) is relative to the wall or to the fluid, a_i and b_i are positive constants, $T_i(0)$ represents the temperatures at the input.

Thus a first approximation, we can assume that, the non linear terms in the energy balance at the receiver (radiative effects) can be neglected. Fig. 2 shows also that, the temperature of the fluid tends to that of the receiving wall and that beyond $L_e \approx 3.5 \text{ m}$, we can assume that, the fluid flow regime is thermally established. It results that, if $L_{conc} \geq L_e$, so $T_f(L_{conc}) \approx T_p(L_{conc}) \approx T_p(L_e)$. Then for this environmental conditions, set the length of the PT to 4.0 m is reasonable because nearly all energy of receiver is recovered by the heat fluid.

On the other hand, when the length of the receiver is less than 2.0 m, the PT is inefficient for solar thermodynamic applications because the output temperature is too low (less than 673 K).

3.3 Influences of the Heat Fluid Flow Rate

Figs. 3 and 4 show the influence of mass flow rate on the heat transfer between the receiver wall, and the heat fluid particularly temperatures change between the wall and the fluid.

Heat transfer from the wall towards the fluid being done by forced convection, the expression of the

coefficient of transfer h_{conv} depends only on Reynolds number Re characteristic of the flow regime.

We considered suitable correlations according to the case. The Re only depends on the mass flow rate \dot{m} with air used as fluid heat considered such as a perfect gas with constant physical properties.

Fig. 3 is laminar flow case, the very low flow rates provide a thermally established regime with relatively high temperatures. In contrast these flow rates do not represent great interest because they are quasi-static, and consequently the quantity of heat collected at output of the tube is insignificant. The range of low

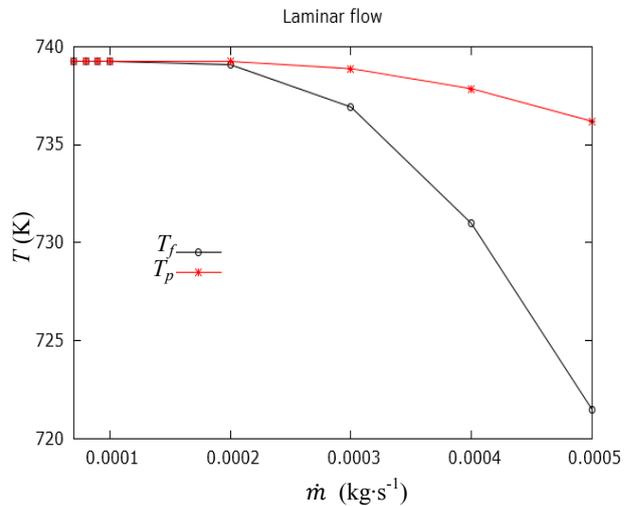


Fig. 3 Evolutions of T_p and T_f according to \dot{m} : laminar flow case ($Re \leq 2,200$).

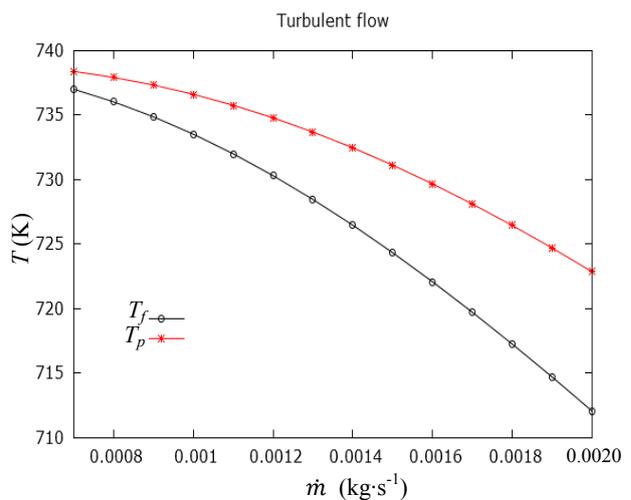


Fig. 4 Evolutions of T_p and T_f according to \dot{m} : turbulent flow case ($Re > 3,000$).

flow rates considered ($\sim 0.3 \times 10^{-3} \text{ kg}\cdot\text{s}^{-1}$ to $0.5 \times 10^{-3} \text{ kg}\cdot\text{s}^{-1}$) shows a large temperature difference between the wall and the fluid (going up to $\sim 15 \text{ }^\circ\text{C}$).

Fig. 4 is turbulent flow case, the temperature difference between the wall and the fluid is minimal for low to moderate flows ($0.8 \times 10^{-3} \text{ kg}\cdot\text{s}^{-1} \leq \dot{m} < 1.4 \times 10^{-3} \text{ kg}\cdot\text{s}^{-1}$). In contrast for high flow rates ($\dot{m} \geq 1.8 \times 10^{-3} \text{ kg}\cdot\text{s}^{-1}$), this difference reaches high values in the order of $10 \text{ }^\circ\text{C}$.

For this type of system, the turbulent flow regime for exchanges by forced convection between the wall receiver and the fluid is the most favorable, but the rates of flow must be moderate or low [2]. This is what led us to work thereafter with rate mass flow \dot{m} of $0.001 \text{ kg}\cdot\text{s}^{-1}$.

3.4 Sample Application Choice of Solar Tangor Sensor

The previous results have allowed us to adopt the solar tangor sensor (Fig. 5).

The solar tangor sensor is constituted by an absorbent cavity with superficial treatment with very high absorption. The absorber is protected by a coaxial borosilicate envelope tube with stagnant air, and very low iron content which prevents the dispersion of heat into the atmosphere. Geometric and optical characteristics of the PT are recorded in Table 1.

The evolutions of the DNI and the output temperature of the fluid $T_f(L_{conc}) = T_{out}$ during a typical day of April (the sunniest month) are given in Fig. 6 [15].

The evolutions of the DNI and the output temperature T_{out} are similar, indicating that, the power received by the receiving surface is the most important factor on the performances of the system. A maximum temperature of 733 K is reached with a DNI of $799 \text{ W}\cdot\text{m}^{-2}$.

Fig. 7 is a 3D representation of the receiver wall temperatures T_p depending on the "Time" and along the receiver tube x . The example is taken for a typical day of April. Output temperatures are highest between



Fig. 5 Solar tangor sensor.

Table 1 PT characteristics.

Parameters	Values
L_{conc}	4.10 m
l_{conc}	1.25 m
l_r	$5.2 \times 10^{-2} \text{ m}$
P_m	$3.4 \times 10^{-2} \text{ m}$
K_{PT}	0.85

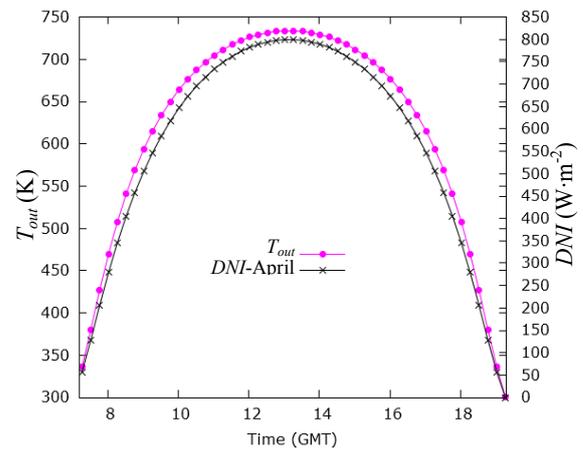


Fig. 6 Evolutions of the DNI and T_{out} during typical day of April.

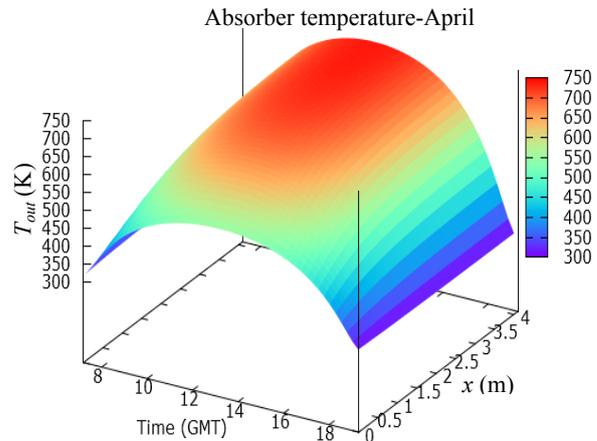


Fig. 7 Profile of T_p in 3D during April.

11 GMT and 15 GMT, and can reach 736 K allowing heating the fluid for thermodynamic use.

The air as a heat transfer fluid is free, simple and reliable for use with a reduced danger, and has little environmental impact. But like a lot of gas, it has a low capacity for heat transfer and its flow causes a lot of energy dissipations [16]. PT performances can be improved by preheating the input temperature of the fluid T_{in} .

4. Conclusions

We have studied the influences of certain parameters on the behavior of a PT using the climatic conditions of Senegal. The solar resource in Senegal particularly during the sunniest season such as in April makes it easy to get temperatures superior to 673 K, preliminary specifications for PT. Thermal storage or hybridization with another energy source is required in case of deficiency of radiation.

The concentrator must be composed of well reflective materials with high transmittance coefficient and protected against damage with better technical and economic compromise. The blocks must be properly assembled to avoid the geometrical losses and well set in tracking to avoid imperfections which can affect its operation.

The absorber must be a perfect conductor painted in black and be protected to prevent heat losses. Thus, the efficiency of the solar conversion to usable heat shall be improved.

It appears from this study, that to have output fluid temperatures usable for applications in thermodynamic solar, the length of the PT must be greater than 2.0 m in our climatic conditions. Also the optimal length of the PT can be set at 4.0 m, because the longitudinal temperature variations of the PT and of the receiver are substantially zero beyond this length.

For this type of system, the turbulent flow regime for the transfer by forced convection between the wall and the fluid is more favorable, but the flow rates

should be moderate or low.

The obtained results which depend on the model are encouraging, so it remains to test its validity in real situation. However, they are indicators that may lead to further studies such as improved optical and geometrical properties of the sensor.

The study of other specific components of a parabolic trough system is the next step in order to design a mini solar power plant, and to make a comparison with a PV system, biogas or diesel.

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